Redesigning of the heating chamber of the Resin Line:
A Case Study

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Abstract: Resin Line is a stone machinery, in which marble & granite slab reinforcement is done. The reinforcement in done by applying epoxy resin on the slab surface and heat it in a heating chamber number of slab are staked in the heating chamber. Thus the height of the heating chamber is reasonably high in the range of 6-8m.

For maintaining homogeneous temperature in the heating chamber which will produce good quality marble slabs a blower and heater system is used. The hot air from the blower-heater system is supplied to the heating chamber through square cross sectional hollow columns. In all there are six column used in manufacturing of heating chamber. In each column there forty holes of the same diameter. These holes in the first three columns are use to supply the hot air into the heating chamber and the remaining holes of the three columns are used for suction the hot air from the heating chamber.

The practical problem faced by the resin line manufacturing industry is to maintain the homogeneous in a 3.5X2.1X6 m sized heating chamber. The temperature near the entrance of the hot air into the heating chamber at the bottom was observed to be 45°C while it was gradually decreasing and reached up to 40°C at the top of the heating chamber. So the qualities of the reinforcement of the marble slabs which are cured at the top of the heating chamber have inferior quality then the slabs at the bottom of the heating chamber. In this situation a very simple but powerful redesigning is done to overcome the above cited problem. In this case study the solution of the problem is obtained by simply increasing the hole diameters gradually from bottom to top keeping total area of the holes same so that blower heater assembly remains same as earlier. In this way the homogenous temperature of 45°C has been achieved throughout the heating chamber from top to bottom, which in turn gives assured quality of marble slabs reinforcement.

Keywords: R.L.M. (Resin Line machine), T.T. (Tilting trolley), VU (Vacuum Unit), RP (Resin Platform), L (Lift), HC (Heating Chamber), TSP (Touch Screen panel)

I. Introduction of Resin Line:

The history of use of marble can be seen in the ancient & antique sculptures made by ancient emperors. In the era of industrialization many types of marble machinery came into existence but in the period of liberalization and globalization the marble slabs being a natural material faces ironical challenges for its cracks & defects.

These defects of the marble can be filled by epoxy resin manually & left for drying & polymerization in open sunlight. But as soon as the weather changes the sunlight goes dim, and the marble industry faces extreme challenges of on-time delivery to the customers hear large space many workers and lot of time dependency of weather halt the on-time delivery of the marble to the valuable customer.

Thus an idea of the resin line machine comes to the mind of the dignitaries of the B.M. industries and India’s first automatic resin line for marble & granite can into existence at B.M. industries Chittorgarh. It is presently engaged in manufacturing resin line-29. This machine requires (1) Less Space (2) Less Workers (3) Less Time (4) Less running cost (5) Weather independent operation.

II. Working & Construction

Main Parts of Resin Line
1) Tilting Trolley
2) Vacuum Unit
3) Resin Platform
4) Lift
5) Heating Chamber
6) Touch Screen Panel
2.1 Tilting Trolley

Automatic loading/unloading procedure of the stone, automatic lifts for the handling of the trays and automatic preparation of the resin are the main points that maximizes the production of the new BM line with only 2 operators for the complete line. All the lines can be customized regarding the dimensions of the trays, the height of the tower and the length according to the available dimensions of the area to be installed.

Slab Loading Unloading Operation By Tilting Trolley For Lesser Worker Fatigue & Time Saving.

2.2 Vacuum Unit

The vacuum chamber is forcing the resin to penetrate in the smallest cracks. Double high capacity vacuum pumps achieves almost absolute air vacuum (-0.8 to -0.9 Bar) in less than 30sec and the slab remains in the vacuum chamber for 60 more seconds. The slab will remain in the chamber between 1’ & 1 1/2’ min without causing any delay in the operation cycle of the complete line.

2.3 Resin Platform

Flexibility & adaptability to any stone or type of treatment is the characteristic of the new BM line, making the line appropriate for all the stones. The productivity and the level of automation can be customized to the needs of every application separately, taking in mind the space and the combination of the line with the polishing lines installed. Slabs & tiles can be treated in the same line. The operation of the line is based on the following steps

Unlike other epoxies ASII20 Instant Install will not stick to the polished surface on granite, allowing for E-Z clean-up with no more taping off joints. It can be colored to match your granite with a coloring kit, but it does dry water clear! Allstone ASII20 Instant Install is a mercaptan epoxy which has different physical characteristics than other epoxies in that it isn’t weather or climate sensitive! It will cure fast in hot or cold temperatures, whether it is humid or arid!

Strongest bond, For lamination & seams of Granite or Natural Stone, Dries fast even in cold temperatures, Stays flexible, Will not fall, crack, shrink, or stain the stone
C₅H₁₀O₂ Molecules with molecular formula

2.4 : Lift
   High speed positioning Lift with continues control of its position through linear encoder and driving system of the trays in the heating chamber. The Lift is self adjusted regarding to the trays position eliminating any operator intervention.
   Vertical Movement of Lift for Dragging & Pushing of Slab at appropriate Position.
   Side View of Lift

2.5 : Heating Chamber
   When the slab reaches the stocking area is completely dry and with the necessary heating energy stored as long as it will remain out of the heating chamber. At the stocking area the steam absorption system removes from the operation area the gases which are produced by the contact of the resin with the hot stone. The optional resin dosing and mixing pump guarantees the correct dosing and mixing of the resin eliminating any operator fault.
   The trays of the slabs are constructed in a way to avoid any deformation from the heating and the weight that are carrying. They are constructed in three dimensions 3200x2000mm that can carry slabs of any kind and strips. Compact Design for Pre & Final Heating of Slab at Appropriate Temperature. Heating & Ducting System Designed for Uniform Heat Treatment & Lower Energy Losses.

III. REDESIGNING OF HEATING CHAMBER

3.1

\[ A_t = 120A_1 \]

\[ A_1 = \frac{\pi d^2}{4} \]

\[ A_t = \frac{\pi d^2}{4} (20)^2 = 314 \text{mm}^2 \]

\[ A_t = 120A_1 = 120 \times 314 = 37680 \text{mm}^2 \]

Existing Heating Chamber having normal circular holes of same size

\[ A_t (\text{Total Area}) = \left[ 40 \times \left( \frac{\pi d_1^2}{4} + \frac{\pi d_2^2}{4} + \cdots + \frac{\pi d_n^2}{4} \right) \right] \times 3 \]

Given

\[ d_1 = 5 \text{mm}, \quad d_2 = 5.5 \text{mm}, \quad d_n = 24.5 \text{mm} \]

\[ A_t (\text{Total Area}) = 37680 \text{mm}^2 \]

Formula for arithmetic progression \[ T_n = a + (n - 1)d \]

Where

\[ a = 5, \quad n = 40, \quad d = 0.5 \]

\[ T_n = 5 + (40 - 1)0.5 = 24.5 \text{mm} \]

Redesigning Heating Chamber using Gradually increasing Circular Hole

\[ A_t (\text{Total Area}) = N \times A_1 (\text{Area of single hole}) \]

Let \[ d = 30 \]

\[ A_1 = \frac{\pi d^2}{4} = \frac{\pi (30)^2}{4} = 706.5 \text{mm}^2 \]

\[ A_t = 37680 \text{mm}^2 = N \times A_1 \]

\[ N = 37680/706.50 = 53.33 \text{ say } 54 \]

Therefore Number of holes in one column (n) = N/3 = 54/3 = 18

Redesigning Heating Chamber using Circular Hole enlarged size.
### Redesigning of the heating chamber of the Resin Line: A Case Study

#### (3.2) Redesigning Heating Chamber using Circular Hole of diminished size

<table>
<thead>
<tr>
<th>Area of single hole</th>
<th>Area of single hole in one column</th>
</tr>
</thead>
<tbody>
<tr>
<td>$A_1 = \pi d^2 = \pi (10)^2$</td>
<td>$78.50 \text{mm}^2$</td>
</tr>
<tr>
<td>$A_1 = 120X314 = 37680 \text{mm}^2$</td>
<td>$A_2 = 78.50$</td>
</tr>
</tbody>
</table>

Therefore Number of holes in one column $N = \frac{A_1}{A_2} = \frac{37680}{78.50} = 480$

Redesigning Heating Chamber using Circular Hole of diminished size

#### (3.3) Number of holes in one column

$$N = \frac{37680}{78.50} = 480$$

#### (3.4) Redesigning Heating Chamber using Normal Circular Hole of same size with dual entry of hot air size

<table>
<thead>
<tr>
<th>Area of single hole</th>
<th>Area of single hole in one column</th>
</tr>
</thead>
<tbody>
<tr>
<td>$A_1 = \pi d^2 = \pi (20)^2$</td>
<td>$314 \text{mm}^2$</td>
</tr>
<tr>
<td>$A_1 = 120X314 = 37680 \text{mm}^2$</td>
<td>$A_2 = 314$</td>
</tr>
</tbody>
</table>

Redesigning Heating Chamber using Normal Circular Hole of same size with dual entry of hot air size

#### (3.5) Redesigning Heating Chamber using Normal Circular Hole of same size with triple entry of hot air

<table>
<thead>
<tr>
<th>Area of single hole</th>
<th>Area of single hole in one column</th>
</tr>
</thead>
<tbody>
<tr>
<td>$A_1 = a^2 = (17.72)^2$</td>
<td>$314 \text{mm}^2$</td>
</tr>
<tr>
<td>$A_1 = 120X314 = 37680 \text{mm}^2$</td>
<td>$A_2 = 314$</td>
</tr>
</tbody>
</table>

Redesigning Heating Chamber using Normal Circular Hole of same size with triple entry of hot air

#### (3.6) Redesigning Heating Chamber using Square Hole of same size

<table>
<thead>
<tr>
<th>Area of single hole</th>
<th>Area of single hole in one column</th>
</tr>
</thead>
<tbody>
<tr>
<td>$A_1 = \frac{1}{2} b \times h = \frac{1}{2} (20 \times 31.4)$</td>
<td>$314 \text{mm}^2$</td>
</tr>
<tr>
<td>$A_1 = 120X314 = 37680 \text{mm}^2$</td>
<td>$A_2 = 314$</td>
</tr>
</tbody>
</table>

Redesigning Heating Chamber using Square Hole of same size

#### (3.7) Redesigning Heating Chamber using Triangular Hole of same size

<table>
<thead>
<tr>
<th>Area of single hole</th>
<th>Area of single hole in one column</th>
</tr>
</thead>
<tbody>
<tr>
<td>$A_1 = \frac{1}{2} b \times h \times \sin(30)$</td>
<td>$4.312 \text{mm}^2$</td>
</tr>
<tr>
<td>$A_1 = 120X314 = 37680 \text{mm}^2$</td>
<td>$A_2 = 314$</td>
</tr>
</tbody>
</table>

Redesigning Heating Chamber using Triangular Hole of same size

### IV. ANALYSIS

#### 4.1: Observation Table for measurement of temperature, pressure and volume of existing heating chamber of resin line and redesign heating chamber of resin line:

<table>
<thead>
<tr>
<th>S. No</th>
<th>Hole number</th>
<th>Temperature (°C)</th>
<th>Pressure (mmHg)</th>
<th>Volume (m³)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Existing</td>
<td>Redesigned</td>
<td>Existing</td>
<td>Redesigned</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>1</td>
<td>1</td>
<td>45</td>
<td>20</td>
<td>52.92</td>
</tr>
<tr>
<td>2</td>
<td>10</td>
<td>44</td>
<td>19</td>
<td>52.92</td>
</tr>
<tr>
<td>3</td>
<td>20</td>
<td>43</td>
<td>18</td>
<td>52.92</td>
</tr>
<tr>
<td>4</td>
<td>30</td>
<td>41</td>
<td>17</td>
<td>52.92</td>
</tr>
<tr>
<td>5</td>
<td>40</td>
<td>40</td>
<td>16</td>
<td>52.92</td>
</tr>
</tbody>
</table>

### 4.2 Formulae for Calculations

- $A_t = NXA_1$ (Area of single hole)
- $A_1 = \pi d^2 = \pi (10)^2 = 78.50 \text{mm}^2$
- $A_1 = 120X314 = 37680 \text{mm}^2$
- $A_t = 37680 \text{mm}^2$
- $A_2 = 78.50$
- $N = \frac{A_1}{A_2} = \frac{37680}{78.50} = 480$
- $A_2 = 314$
- $A_1 = \frac{1}{2} b \times h = \frac{1}{2} (20 \times 31.4)$
- $A_1 = 120X314 = 37680 \text{mm}^2$
- $A_2 = 314$
- $A_1 = a^2 = (17.72)^2$
- $A_1 = 120X314 = 37680 \text{mm}^2$
- $A_2 = 314$
- $A_1 = \frac{1}{2} b \times h \times \sin(30)$
- $A_1 = 120X314 = 37680 \text{mm}^2$
- $A_2 = 314$
- $A_1 = \frac{1}{2} b \times h \times \sin(30)$
- $A_1 = 120X314 = 37680 \text{mm}^2$
- $A_2 = 314$
- $Q = a \times v$
- $PV = RT$

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\[
\left(\frac{40}{\pi} \left( \frac{d_1^2}{4} + \frac{d_2^2}{4} + \ldots + \frac{d_n^2}{4} \right) \right) \times 3
\]

Formula for arithmetic progression \( T_n = a + (n-1)d \)

\( A_t(\text{Total Area}) = NXA_1 \) (Area of single hole)

\[ A_t(\text{Total Area}) = 120XA_i \]

\[ Q^* = kA\frac{dT}{Ax} \]

\[ \eta = \frac{\Delta T}{\Delta x} \]

\[ \rho = \frac{v^2}{2g} + h = C \]

4.3 : OUTCOME SUMMARY

<table>
<thead>
<tr>
<th>S. No.</th>
<th>Description</th>
<th>Dimension (mm)</th>
<th>Area of a Single hole (mm²)</th>
<th>Total Area (mm²)</th>
<th>Number of holes in one column</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.</td>
<td>Normal Circular Hole of same size</td>
<td>d=20</td>
<td>314</td>
<td>37680</td>
<td>40</td>
</tr>
<tr>
<td>2</td>
<td>Gradually increasing Circular Hole</td>
<td>( d_1=5, d_2=5.5, d_n=24.5 )</td>
<td>-</td>
<td>37680</td>
<td>40</td>
</tr>
<tr>
<td>3</td>
<td>Circular Hole enlarged size.</td>
<td>d=30</td>
<td>( A_1=706.5 )</td>
<td>37680</td>
<td>18</td>
</tr>
<tr>
<td>4</td>
<td>Circular Hole of diminished size</td>
<td>d=10</td>
<td>( A_1=78.5 )</td>
<td>37680</td>
<td>160</td>
</tr>
<tr>
<td>5</td>
<td>Normal Circular Hole of same size with dual entry of hot air</td>
<td>d=20</td>
<td>314</td>
<td>37680</td>
<td>40</td>
</tr>
<tr>
<td>6</td>
<td>Normal Circular Hole of same size with triple entry of hot air</td>
<td>d=20</td>
<td>314</td>
<td>37680</td>
<td>40</td>
</tr>
<tr>
<td>7</td>
<td>Square Hole of same size</td>
<td>a=17.72</td>
<td>314</td>
<td>37680</td>
<td>40</td>
</tr>
<tr>
<td>8</td>
<td>Triangular Hole of same size</td>
<td>b=20, h=31.4</td>
<td>314</td>
<td>37680</td>
<td>40</td>
</tr>
</tbody>
</table>

4.4 : Graph

**Hole Dimension**
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4.5 : Result Analysis

<table>
<thead>
<tr>
<th>S. No.</th>
<th>Description*</th>
<th>Remarks</th>
<th>Feasibility</th>
</tr>
</thead>
<tbody>
<tr>
<td>1.</td>
<td>Normal Circular Hole of same size</td>
<td>Existing heating chamber</td>
<td>Yes</td>
</tr>
<tr>
<td>2.</td>
<td>Gradually increasing Circular Hole</td>
<td>Redesigned heating chamber practically accepted by the owner of B.M. Industries</td>
<td>Yes</td>
</tr>
<tr>
<td>3.</td>
<td>Circular Hole enlarged size</td>
<td>Non uniform heating</td>
<td>No</td>
</tr>
<tr>
<td>4.</td>
<td>Circular Hole of diminished size</td>
<td>Too much holes, weaker column</td>
<td>No</td>
</tr>
<tr>
<td>5.</td>
<td>Normal Circular Hole of same size with dual entry of hot air</td>
<td>Blower power increases which in turn increases initial cost of the machine</td>
<td>No</td>
</tr>
<tr>
<td>6.</td>
<td>Normal Circular Hole of same size with triple entry of hot air</td>
<td>Blower power increases which in turn increases initial cost of the machine</td>
<td>No</td>
</tr>
<tr>
<td>7.</td>
<td>Square Hole of same size</td>
<td>At the corner of the square hole stress concentration, design failure</td>
<td>No</td>
</tr>
<tr>
<td>8.</td>
<td>Triangular Hole of same size</td>
<td>At the corner of the triangular hole stress concentration, design failure</td>
<td>No</td>
</tr>
</tbody>
</table>
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Before

After

Fig. : Variation of Temperature in Heating Chamber

Fig. : Variation of Temperature in Heating Chamber
Redesigning of the heating chamber of the Resin Line: A Case Study

Before

After

Variation of Pressure

Variation of Volume
V. Conclusion:
The Existing heating chamber of the resin line was not maintained at homogenous temperature of 45°C for slab reinforcement. After redesigning the heating chamber the homogenous temperature of 45°C has been achieved just by gradually varying the hole dimensions of the columns of the heating chamber.

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References: